



PAD FOOTING V5.12

Engineering Building & Infrastructure Pty Ltd

Pad:	(Pad Footing PF01) 1200mm long x 1200mm wide, 700mm deep, f'c = 120MPa	
	Bearing = 48928kPa < 212850kPa	OK (0.23)
Reinf't:	N50-100 cts (BLL), 35-N50/m [29 cts] (BUL) (BLL bars in L dir.), 100mm cover	
Capacity:	M*L = 3360.1kNm/m < ϕMu.L = 4288.8kNm/m, M*W = 6425.1kNm/m < ϕMu.W = 9092.5kNm/m	OK (0.78,0.71)
	V*L = 0.0kN/m < ϕVuc.L = 370.3kN/m, V*W = 0.0kN/m > ϕVuc.W = 365.5kN/m	OK (0.00,0.00)
	VP* = 2010kN < ϕVp = 6296kN	OK (0.32)
Column:	800mm long x 450mm wide, P* = 94508kN	

Geometry (Designing at asup from column centreline)

Two-way slab footing

Concrete strength (f'c) =	120 MPa	Column length (CL) =	800 mm
Pad length (L) =	1200 mm	Column width (CW, CW=0 for Circle) =	450 mm
Pad width (W) =	1200 mm	Column area reduction =	1.41 m ²
Pad depth (D) =	700 mm	Outstand in L direction =	200 mm
Design moment at column face =	N (Y)es,(N)o	Outstand in W direction =	375 mm
Use asup (=0.7) =	Y (Y)es,(N)o	Pad Area =	1.44 m ²
Method =	E (E)lastic/(P)lastic		

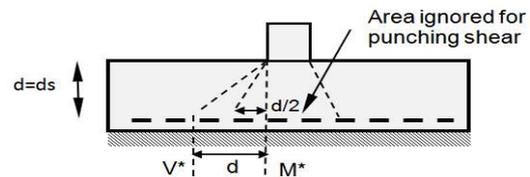
Loading

Dead load (Pdl) = 70000 kN (Excluding footing S.Wt)
Live load (PlI) = 450 kN

Eccentricity (EccL) = 0 mm
Eccentricity (EccW) = 0 mm

S.Wt. density (ρ) = 6.0 kN/m³
S.Wt. = ρ*L*W*D = 6.0 kN
P* = 1.35*(Pdl+SWt) = 94508 kN
(Bearing elastically determined)

Allowable bearing pressure = 212850 kPa
Max. bearing pressure (Bp) = 48928 kPa



OK (0.23)
Ultimate B.P.(Bp*) = 65631 kPa
P*/Rt = 1.3414

Reinforcement

Unreinforced = N (Y)es, (N)o
Extreme bottom bars in = L (W), (L) dir
Cover to bottom layer of reinf't = 100 mm

Bottom reinf't layers = 1
Ductility class = A (N)ormal,(L)ow,(A)uto
Ductility class = N (N)ormal,(L)ow

BLL (in L dir.) = N50-100 cts (BLL)

Bar size = 50 mm
Bar cts/No. per m = 100 mm
Steel Strength (fsy) = 500 MPa
Area steel (Ast) = 19635 mm²/m
Depth to steel (ds) = 575 No
Ast.min = 0.19*(D/ds)²*f'ct.f/fsy*ds = 2128 mm²/m

BUL (in W dir.) = 35-N50/m [29 cts] (BUL)

Bar size = 50 mm
Bar cts/No. per m = 35 No/m
Steel Strength (fsy) = 500 MPa
Area steel (Ast) = 68722 mm²/m
Depth to steel (ds) = 525 No
Ast.min = 2331 mm²/m

Bending (Reinforced) - Cl 8.1 (Applicable)

alpha (α2 = 0.85-0.0015*f'c) =	0.670 (0.67 ≤ α2)	Eq 8.1.3(1)	
gamma (γ = 0.97-0.0025*f'c) =	0.670 (0.67 ≤ γ)	Eq 8.1.3(2)	
Strength factor (ϕbl = 1.24-13*kuo/12) =	0.85	ϕbw =	0.85 (0.65 ≤ ϕ ≤ 0.85) Table 2.2.2 for N Class
Moment (ML*) =	3360.1 kNm/m	MW* =	6425.1 kNm/m
Ast Req'd =	14960 mm ² /m	Ast Req'd =	36830 mm ² /m
ϕMuo.L =	4288.8 kNm/m	ϕMuo.W =	9092.5 kNm/m
	OK (0.78)		OK (0.71)

Bending (Unreinforced) - Cl 20.4.2 (Not applicable)

Plain concrete (ϕ.ur) = 0.6 Table 2.2.2(g)
ϕMuo.ur.L = (ϕ=0.6)*f'ct.f*Z = 277.7 kNm/m **No Good (12.10)**
ϕMuo.ur.W = 277.7 kNm/m **No Good (23.14)**



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Punching shear (Reinforced) - Cl 9.3 (Applicable)

Pad load (P*) =	94508 kN	dom =	525 mm	
Column load reduction =	92498 kN	Perim. (u) =	4600 mm	
Punching shear (Vp*) =	2010 kN	βh =	1.8	Cl 9.3.1.4
		fcv =	3.72 MPa	Cl 9.3.3
$\phi V_p = (\phi=0.7) * u * dom * f_{cv} =$	6296.3 kN		OK (0.32)	

Punching shear (Unreinforced) - Cl 20.4.3 (Not applicable)

Punching shear (Vp*) =	2010 kN	
$\phi V_{p.ur1} = (\phi=0.6) * 0.1 * u * (D-50) * (1+2/\beta h) * v_{f'c} =$	4176.1 kN	
$\phi V_{p.ur2} = (\phi=0.6) * 0.2 * u * (D-50) * v_{f'c} =$	3930.5 kN	
$\phi V_{p.ur} = \min(\phi V_{p.ur1}, \phi V_{p.ur2}) =$	3930.5 kN	OK (0.51)

Strength of slab in one-way shear (Reinforced) - Cl 8.2 (Applicable)

Use Simplified method =	N (Yes,(N)o			
Max. nominal aggregate size (dg) =	16 mm	(General method)		
Lightweight concrete =	N (Yes,(N)o	(General method)		
	Length		Width	
1-way shear (VL*) =	0.0 kN/m	VW* =	0.0 kN/m	
ML* =	0.0 kNm/m	MW* =	0.0 kNm/m	
ds =	575 mm	ds =	525 mm	
Effective shear depth $d_v = \max(0.72 * D, 0.9 * ds) =$	518 mm	d_v =	504 mm	Cl 8.2.1.9
Total flange (W) =	1200 mm	L =	1200 mm	
Effective flange (bv) =	1000 mm	bv =	1000 mm	
Simple method for kv & θv - Cl 8.2.4.3				
$k_{vo} = 200 / (1000 + 1.3 * d_v) =$	0.120	$k_{vo} =$	0.121	
$k_v = \min(k_{vo}, 0.15) =$	0.120	$k_v =$	0.121	Eq 8.2.4.3(1)
Angle of inclination of concrete comp. strut (θv) =	36.0 °	$\theta_v =$	36.0 °	
General method for kv & θv - Cl 8.2.4.2				
Tensile area of concrete (Act) =	350000 mm ² /m	Act =	350000 mm ² /m	
Ast =	19635 mm ² /m	Ast =	68722 mm ² /m	
Shear only $\epsilon_{x1} \leq 3000 * 10^{-6} =$	0.0 x10 ⁻⁶	$\epsilon_{x1} =$	0.0 x10 ⁻⁶	Eq 8.2.4.2.2(1)
Shear only $-200 * 10^{-6} \leq \epsilon_{x2} \text{ (where } \epsilon_{x1} < 0) \leq 0 =$	0.0 x10 ⁻⁶	$\epsilon_{x2} =$	0.0 x10 ⁻⁶	Eq 8.2.4.2.2(2)
Long. mid-depth concrete strain (εx) =	0.0 x10 ⁻⁶	$\epsilon_x =$	0.0 x10 ⁻⁶	
kdg = 2.0 =	2.000	kdg =	2.000	Eq 8.2.4.2(4)
$k_v = (0.4 / (1 + 1500 * \epsilon_x)) * (1300 / (1000 + k_{dg} * d_v)) =$	0.256	$k_v =$	0.259	Eq 8.2.4.2(2)
Angle (θv) = (29 + 7000 * εx) =	29.0 °	$\theta_v =$	29.0 °	Eq 8.2.4.2(1)
Adopted kv & θv - General method - Cl 8.2.4.2				
$k_v =$	0.256	$k_v =$	0.259	
Angle of inclination of concrete compression strut (θv) =	29.0 °	$\theta_v =$	29.0 °	
Concrete contribution to shear strength - Cl 8.2.4.1				
Capacity reduction factor (φ) =	0.70	φ =	0.70	Table 2.2.2(e)
$k_v =$	0.256	$k_v =$	0.259	
Effective flange (bv) =	1000 mm/m	bv =	1000 mm/m	
Effective shear depth (dv) =	518 mm	d_v =	504 mm	
$\min(v_{f'c}, 8.0) =$	8.00 MPa	Limited from 10.95MPa - Cl 8.2.4.1		
$V_{uc} = k_v * b_v * d_v * \min(v_{f'c}, 8.0) =$	1057.9 kN/m	$V_{uc} =$	1044.1 kN/m	Cl 8.2.4.1
D ≥ 650mm, ks =	0.50			
$k_s * \phi V_{uc.L} =$	370.3 kN/m	$k_s * \phi V_{uc.W} =$	365.5 kN/m	Eq 8.2.1.6(1)
	OK (0.00)		OK (0.00)	

Strength of slab in one-way shear (Unreinforced) - Cl 20.4.3 (Not applicable)

1-way shear (VL*) =	0.0 kN/m	VW* =	0.0 kN/m
$\phi V_{u.ur.L} = (\phi=0.6) * 0.15 * b * (D-50) * f_{c'}^{1/3} =$	288.5 kN/m	$\phi V_{u.ur.W} =$	288.5 kN/m
	OK (0.00)		OK (0.00)



Total weight (Rt = Pdl + S.Wt + Pll) = 70456.0 kN

Bearing Pressure - Elastic

Bearing pressure B.P. (Rt/[W*L]) = 48927.8 kPa

	Width		Length		
Eccentricity (Ecc.x) =	0	mm	Eccentricity (Ecc.y) =	0	mm
yx = (W/2 - Ecc.x) =	600	mm	yy = (L/2 - Ecc.y) =	600	mm

Bearing pressure (1/A) =	48927.8	kPa	Bearing Distance (1-2) =	1200	mm
Bearing pressure (2/F) =	48927.8	kPa	Bearing Distance (2-3) =	1200	mm
Bearing pressure (3/K) =	48927.8	kPa	Bearing Distance (3-4) =	1200	mm
Bearing pressure (4/P) =	48927.8	kPa	Bearing Distance (4-1) =	1200	mm

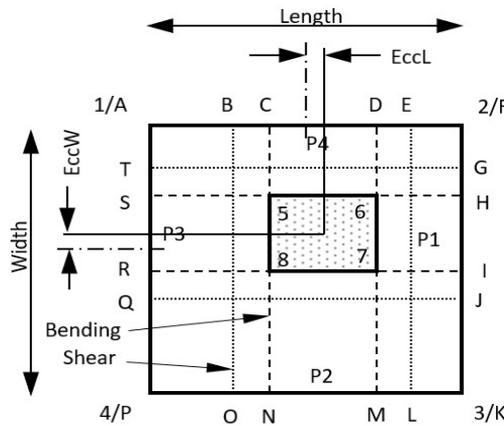
Minimum bearing pressure (q.min) = 48927.8 kPa
 Maximum bearing pressure (q.max) = 48927.8 kPa OK (0.23)

Bearing Pressure - Plastic (Not applicable)

	Width		Length		
Eccentricity (Ecc.x) =	0	mm	Eccentricity (Ecc.y) =	0	mm
Effective width (2*yw) =	1200	mm	Effective length (2*yl) =	1200	mm

Maximum bearing pressure (q.max) = 48927.8 kPa OK (0.23)

Calculations



	Working kPa	Ultimate kPa		Working kPa	Ultimate kPa
1/A	48927.8	65630.7	3/K	48927.8	65630.7
B	48927.8	65630.7	L	48927.8	65630.7
C	48927.8	65630.7	M	48927.8	65630.7
D	48927.8	65630.7	N	48927.8	65630.7
E	48927.8	65630.7	O	48927.8	65630.7
2/F	48927.8	65630.7	4/P	48927.8	65630.7
G	48927.8	65630.7	Q	48927.8	65630.7
H	48927.8	65630.7	R	48927.8	65630.7
I	48927.8	65630.7	S	48927.8	65630.7
J	48927.8	65630.7	T	48927.8	65630.7

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**Design Bending** (Moment and shear reduced by 0.9 * Self-weight)

Dist 1/A - C (L) + Lext = 320 mm Dist 1/A - S (W) = 442.5 mm
 Dist D - 2/F (L) + Wext = 320 mm Dist R - 4/P (W) = 442.5 mm

	Area	Ave BP kPa	Area m ²	Shear kN	Ecc m	Moment kNm	
P1	DFKM	65630.7	0.38	25200.7	0.160	4032.1	L Dir
P2	RIKP	65630.7	0.53	34847.9	0.221	7710.1	W Dir
P3	ACNP	65630.7	0.38	25200.7	0.160	4032.1	L Dir
P4	AFHS	65630.7	0.53	34847.9	0.221	7710.1	W Dir

L Direction (ML*) = 3360.1 kNm/m
 W Direction (MW*) = 6425.1 kNm/m

Design Shear (Moment and shear reduced by 0.9 * Self-weight)

Depth dv (W) = 504 mm
 Depth dv (L) = 504 mm
 VDist 1/A - B (L) = 0 mm VDist 1/A - T (W) = 0 mm
 VDist E - 2/F (L) = 0 mm VDist Q - 4/P (W) = 0 mm

	Area	Ave BP kPa	Area m ²	Shear kN	Ecc m	Moment kNm	
P1	EFKL	0.0	0.00	0.0	0.000	0.0	L Dir
P2	QJKP	0.0	0.00	0.0	0.000	0.0	W Dir
P3	ABOP	0.0	0.00	0.0	0.000	0.0	L Dir
P4	AFGT	0.0	0.00	0.0	0.000	0.0	W Dir

L Direction (VL*) = 0.0 kN/m L Direction (ML*) = 0.0 kNm/m
 W Direction (VW*) = 0.0 kN/m W Direction (MW*) = 0.0 kNm/m



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Pad: (Pad Footing PF01) 1200mm long x 1200mm wide x 700mm deep
 Uplift: $P_{up*} = 100\text{kN} < \phi P_{down} = 63023\text{kN}$ OK (0.00)
 Down: $P_{down} + S.Wt = 70025\text{kN}$, Bearing = $48629\text{kPa} < 212850\text{kPa}$ OK (0.23)

Geometry

Pad length (L) = 1200 mm Slab thickness (th) = 150 mm
 Pad width (W) = 1200 mm Soil thickness = 0 mm
 Pad depth (D) = 700 mm
 Allowable bearing pressure = 212850 kPa
 Concrete density (ρ_c) = 25.0 kN/m³
 Soil density (ρ_s) = 18.0 kN/m³

Loadings

Ultimate uplift load (P_{up*}) = 100.0 kN
 Working downward load (P_{down}) = 70000.0 kN
 Pad self weight ($S.Wt. = \rho_c * L * W * D$) = 25.2 kN
 $P_{down} + S.Wt = 70025.2$ kN
 Max. bearing pressure ($B_p = (P_{down} + S.Wt) / (L * W)$) = 48629 kPa OK (0.23)

Uplift resistance

Overlap = 0 mm footing under the slab in L Direction, -ve for more options

Area of slab for uplift (A_u) = 0.00 m²
 Vertical load $P_{down} = 70000.0$ kN
 Pad self weight $S.Wt. = \rho_c * L * W * D = 25.2$ kN
 Slab self weight $Wt. (A_u * \rho_c * th) = 0.0$ kN
 Soil self weight $Wt. = 0.0$ kN
 $\Sigma P_{down} = 70025.2$ kN
 $\phi \Sigma P_{down} = 0.9 * \Sigma P_{down} = 63022.7$ kN
 Ratio = $P_{up*} / \phi \Sigma P_{down} = \text{OK} (0.00)$

